

$$\Delta\theta\Delta t \ll \frac{\theta_s P}{2\pi} \approx \theta_s \times 1.37 \times 10^4 \text{ s} \quad (3)$$

Example

Like in the previous example, if we want to image an area of $\Delta\theta = 900 \text{ arcsec}$ when $\theta_s = 4 \text{ arcsec}$, the averaging time should be

$$\Delta t \ll \frac{\theta_s}{\Delta\theta} \times 1.37 \times 10^4 \text{ s} = \frac{4 \text{ arcsec}}{900 \text{ arcsec}} \times 1.37 \times 10^4 \text{ s} \approx 60 \text{ s}$$

Note that we are considering here the **correlator integration time**, i.e. the integration time of a single visibility data point. The full image integration time can be practically anything: minutes, hours and even longer if the source structure does not change.

Antenna response:

$$K = \frac{\eta_a A}{2k} 10^{-26} = \frac{A_{eff}}{2k} 10^{-26} = \frac{T_a}{S} \left[\frac{\text{K}}{\text{Jy}} \right] = \text{DPFU} \quad (4)$$

System response **SEFD**: what amount of source flux increases the system noise as much as the noise of the receiving equipment when $T_a = 0$:

$$\text{SEFD} = \frac{T_{sys}}{\text{DPFU}} = \frac{2kT_{sys}}{A_{eff}} \cdot 10^{-26} \quad [\text{Jy}] \quad (5)$$

Baseline sensitivity for antennas i and j ($\eta_s =$ system efficiency):

$$\Delta S_{ij} = \frac{1}{\eta_s} \sqrt{\frac{\text{SEFD}_i \cdot \text{SEFD}_j}{2\Delta\nu\tau_{int}}} \quad [\text{Jy}] \quad (6)$$

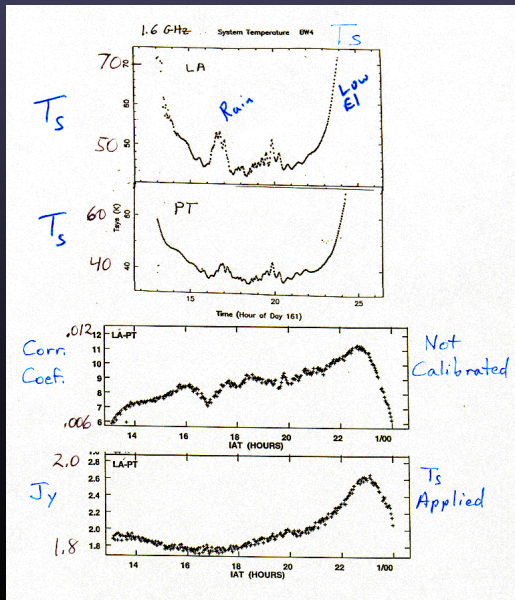
Calibration and imaging



Calibration with system temperatures

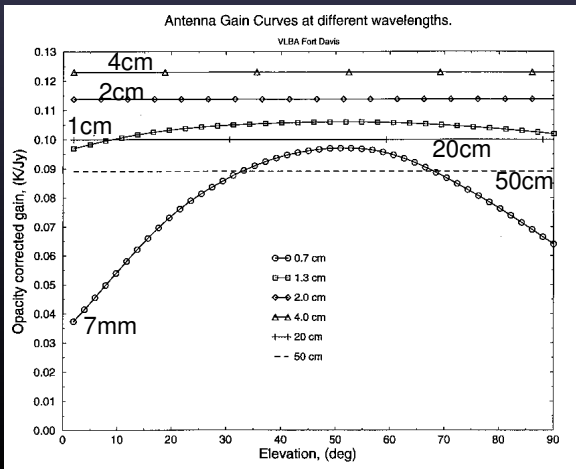
Upper plot: increased T_{sys}
due to rain and low
elevation

Lower plot: removal of the
effect.



VLBA gain curves

- Caused by gravitationally induced distortions of antenna
- Function of elevation, depends on frequency



The phase of a baseline consists of three components:

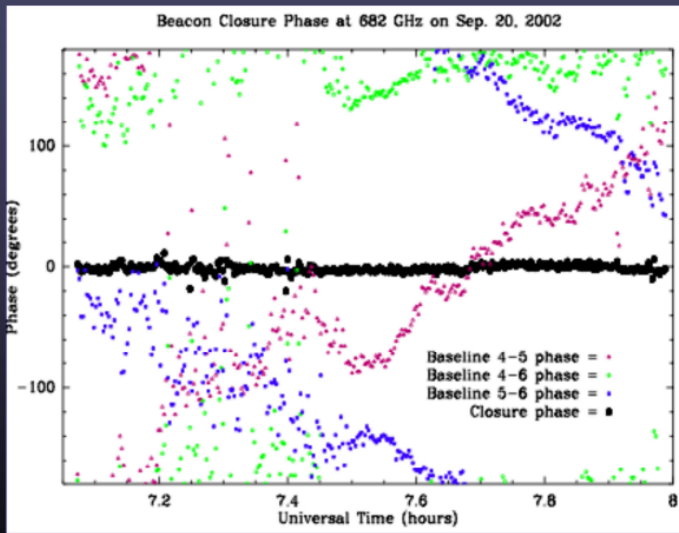
$$\phi_{ij} = \phi_{ij}^{\text{true}} + \phi_i^{\text{err}} - \phi_j^{\text{err}}, \quad (10)$$

i.e. true phase due to the source structure and phase errors of individual antennas.

If we take a sum of phases of three antennas, or a baseline triangle, we get the **closure phase**:

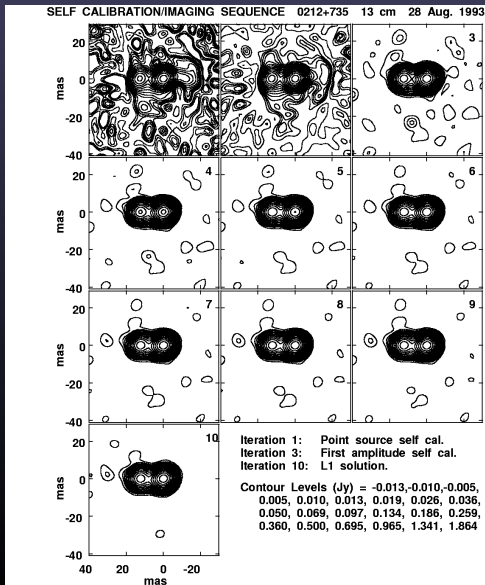
$$\begin{aligned} \Psi_{ijk} &= \phi_{ij} + \phi_{jk} + \phi_{ki} \\ &= (\phi_{ij}^{\text{true}} + \phi_i^{\text{err}} - \phi_j^{\text{err}}) \\ &\quad + (\phi_{jk}^{\text{true}} + \phi_j^{\text{err}} - \phi_k^{\text{err}}) \\ &\quad + (\phi_{ki}^{\text{true}} + \phi_k^{\text{err}} - \phi_i^{\text{err}}) \end{aligned}$$

SMA closure phase measurements at 682GHz



Self calibration imaging sequence

- Iterative procedure to solve for both image and gains:
 - Use best available image to solve for gains (start with point)
 - Use gains to derive improved image
 - Should converge quickly for simple sources
- Does not preserve absolute position or flux density scale



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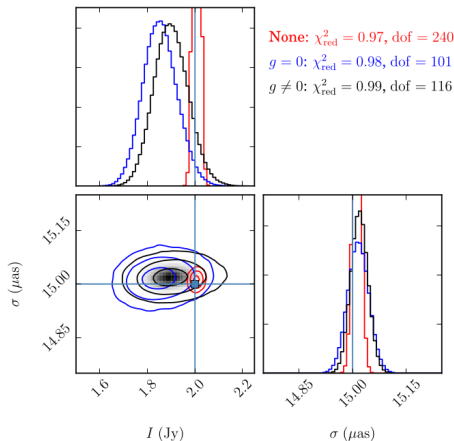
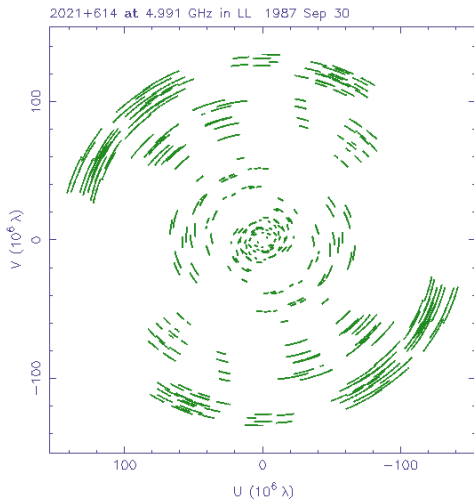
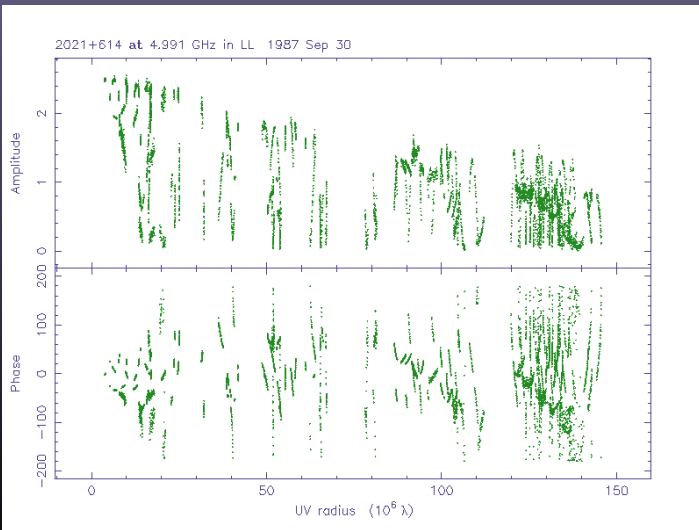


Figure 13. Posterior distribution of the size and amplitude of a symmetric Gaussian reconstructed from simulated visibility amplitude data with $\sigma_0 = 15 \mu\text{as}$ without (red) and with (blue and black) station gain reconstruction. These include the posteriors from simulated data without gain errors (red and blue) and with significant imposed gain errors (black).

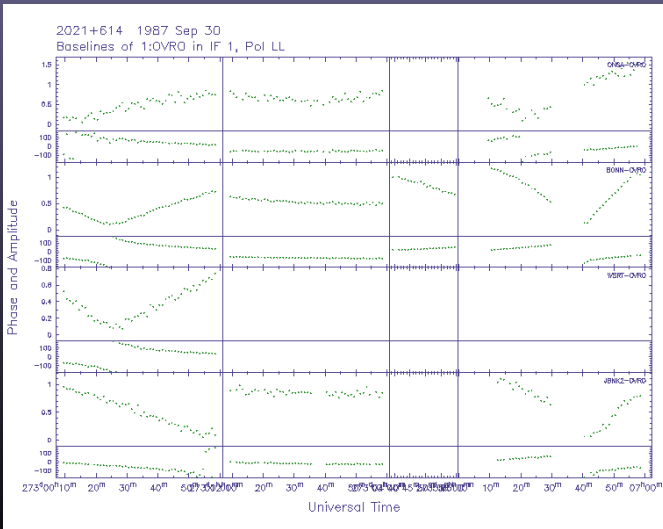
Sampling of the (u,v) plane



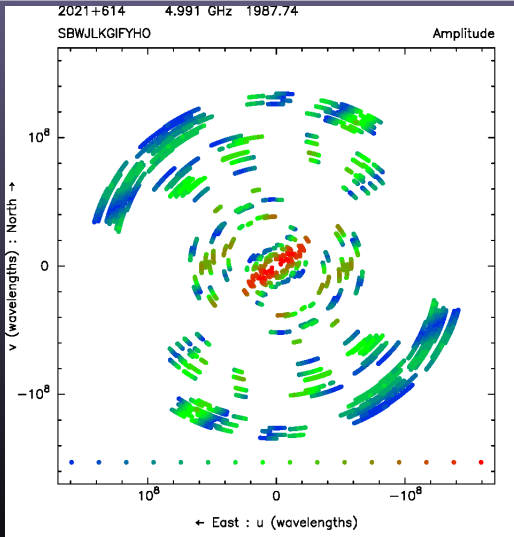
Visibility versus (u,v) radius



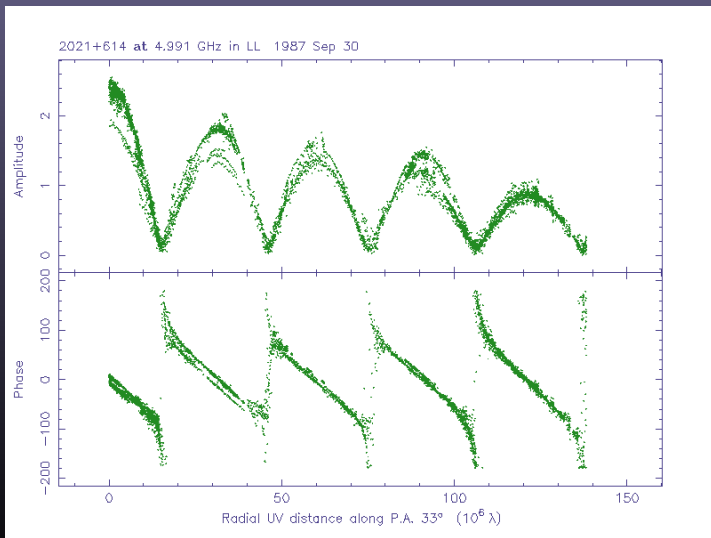
Visibility versus time



Amplitude across the (u,v) plane



Projection in the (u,v) plane



Fourier transform properties

$$F(u, v) = \text{FT}\{f(x, y)\}$$

i.e.,

$$F(u, v) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(x, y) \exp[2\pi i(ux + vy)] dx dy$$

Linearity

$$\text{FT}\{f(x, y) + g(x, y)\} = F(u, v) + G(u, v)$$

Convolution

$$\text{FT}\{f(x, y) \star g(x, y)\} = F(u, v) \cdot G(u, v)$$

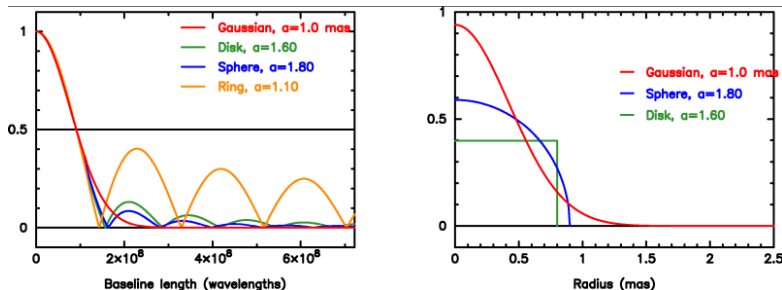
Shift

$$\text{FT}\{f(x - x_i, y - y_i)\} = F(u, v) \exp[2\pi i(ux_i + vy_i)]$$

Similarity

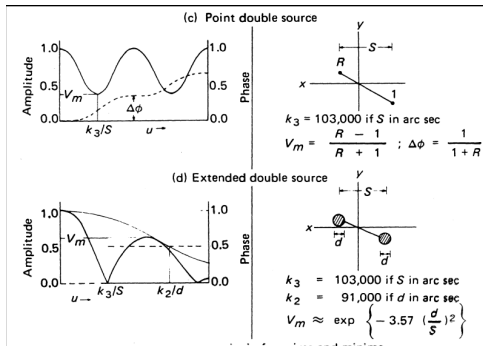
$$\text{FT}\{f(ax, by)\} = \frac{1}{|ab|} F\left(\frac{u}{a}, \frac{v}{b}\right)$$

Component profiles



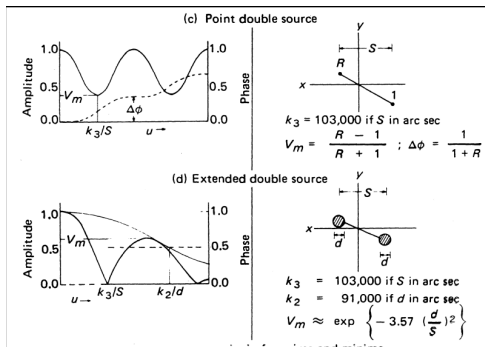
There is very little difference in the uv-plane between different source profiles down to the relative half flux level.

Simple source structures



Component separation from the uv -radius (in wavelengths) of the first valley (k_3/S), size of individual emission region (d [arcsec]) from the uv -radius of the half-value point of the envelope (k_2/d). Amplitude is normalized.

Simple source structures, example



First valley at $100 M\lambda = k_3/S$, envelope half-value point $300 M\lambda = k_2/d$.

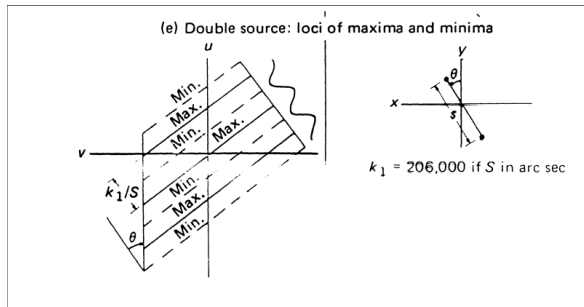
Double source, component separation

$$S = k_3/100M\lambda = 103000/100e6 = 0.001 \text{ arcsec} = 1 \text{ marcsec.}$$

Component size

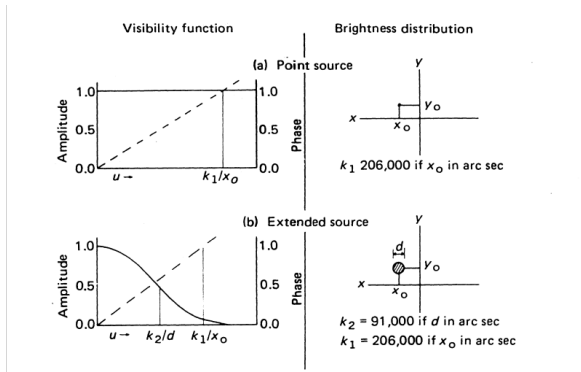
$$d = k_2/300M\lambda = 91000/300e6 = 0.0003 \text{ arcsec} = 300 \mu\text{arcsec}$$

Simple source structures in 2D



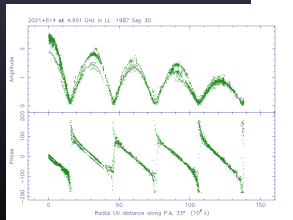
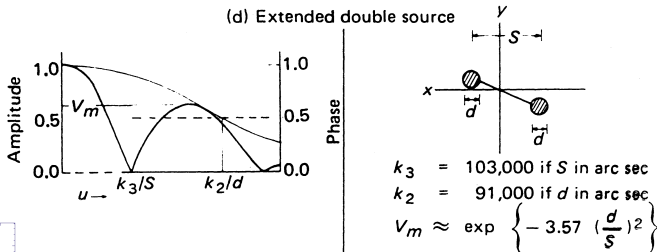
Component separation from the valley-to-valley distance (k_1/S).

Source shift

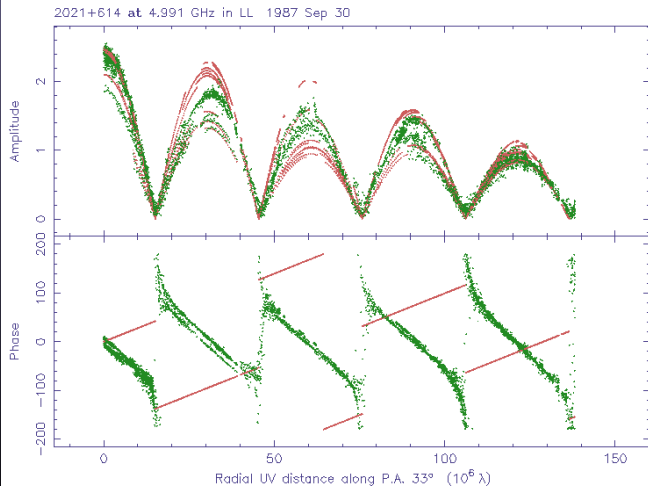


Trial model

- By inspection, we can derive a simple model:
- Two equal components, each 1.25 Jy, separated by about 6.8 milliarcsec in p.a. 33° , each about 0.8 milliarcsec in diameter (Gaussian FWHM)
- *To be refined later.*



Projection in the (u,v) plane



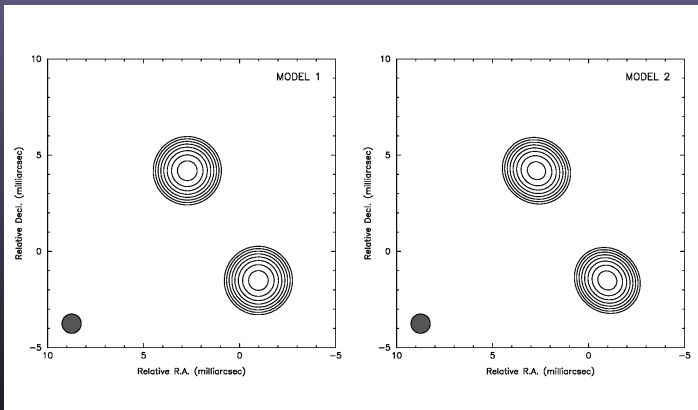
Parameters

- Example
 - Component position: (x,y) or polar coordinates
 - Flux density
 - Angular size (e.g., FWHM)
 - Axial ratio and orientation (position angle)
 - For a non-circular component
 - 6 parameters per component, plus a “shape”

 - This is a conventional choice: other choices of parameters may be better!
 - (Wavelets; shapelets* [Hermite functions])
 - * Chang & Refregier 2002, ApJ, 570, 447

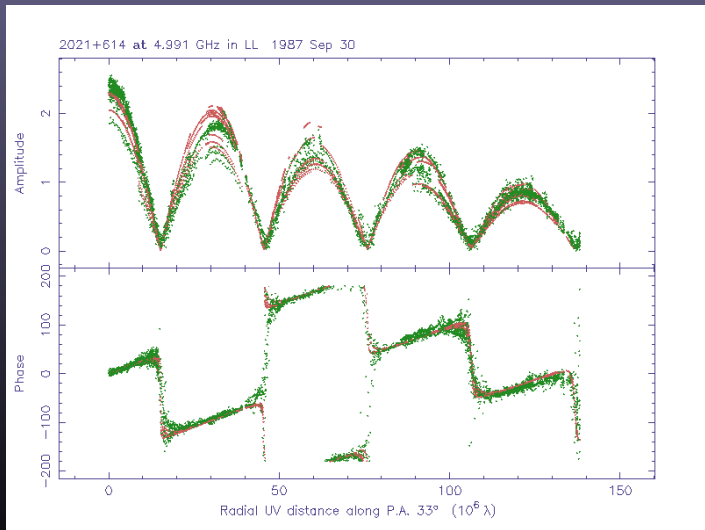


Practical model fitting: 2021

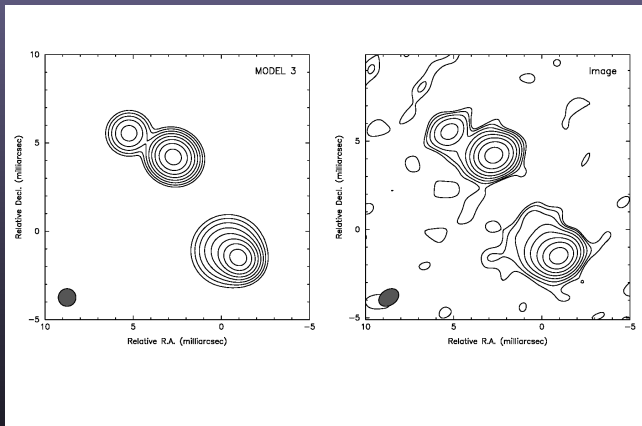


	! Flux (Jy)	Radius (mas)	Theta (deg)	Major (mas)	Axial ratio	Phi (deg)	T
•	1.15566	4.99484	32.9118	0.867594	0.803463	54.4823	1
•	1.16520	1.79539	-147.037	0.825078	0.742822	45.2283	1

2021: model 2

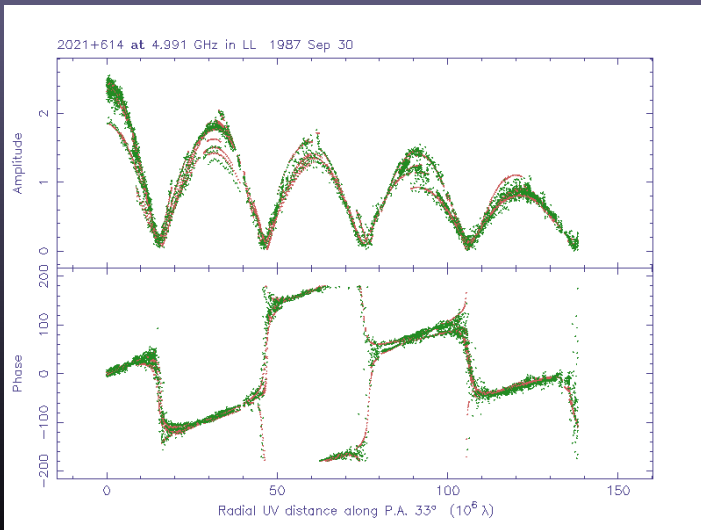


Model fitting 2021

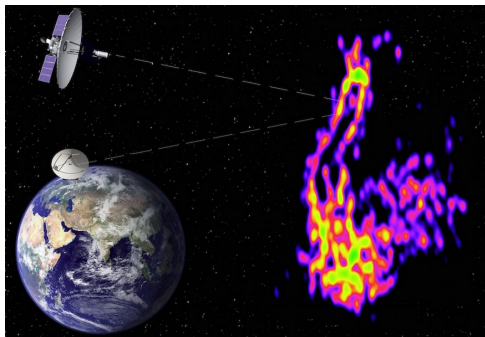


•	! Flux (Jy)	Radius (mas)	Theta (deg)	Major (mas)	Axial ratio	Phi (deg)	T
•	1.10808	5.01177	32.9772	0.871643	0.790796	60.4327	1
•	0.823118	1.80865	-146.615	0.589278	0.585766	53.1916	1
•	0.131209	7.62679	43.3576	0.741253	0.933106	-82.4635	1
•	0.419373	1.18399	-160.136	1.62101	0.951732	84.9951	1

2021: model 3



Example: Space radio interferometry



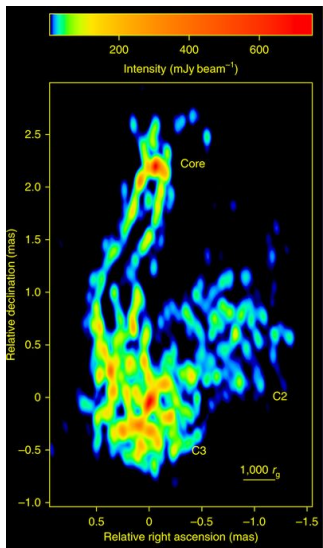
Yhdistämällä useita teleskooppeja toisiinsa pystyttiin ottamaan ennätystarkka kuva mustan aukon suihkusta. Kuva Pier Raffaele Platania INAF/IRA (kompositio); Lebedev Instituutti (RadioAstron)

03.04.2018 | Sakari Nummila

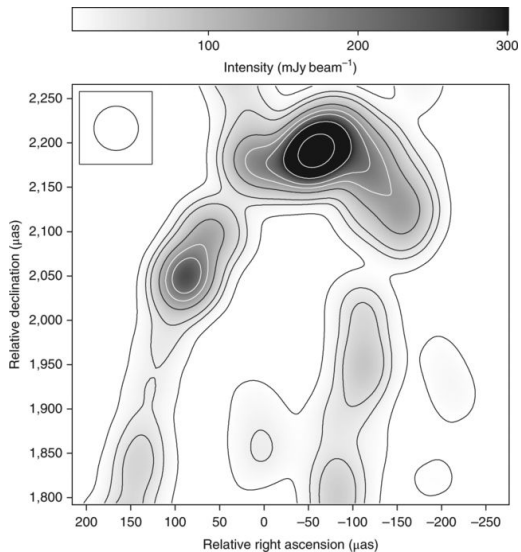
Tähtitieteilijät loivat maapalloa suuremman teleskoopin

Tuomas Savolainen käytti tähtitieteen historian tarkinta havaintolaitetta tutkiakseen mustan aukon synnyttämää plasmasuihkua. Tulokset paljastivat uutta tietoa jäättiläismäisten suihkujen rakenteesta.

Example: Space radio interferometry



Example: Space radio interferometry



Event Horizon Telescope (EHT)

A Global Network of Radio Telescopes



EHT Newsroom: Quest for the Shadow of a Black Hole



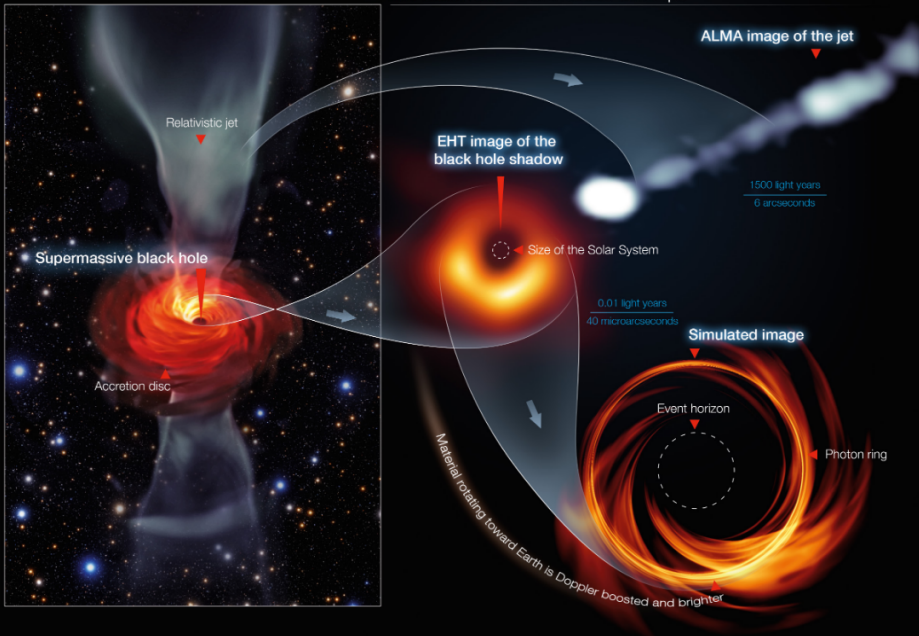
[Download Image](#)

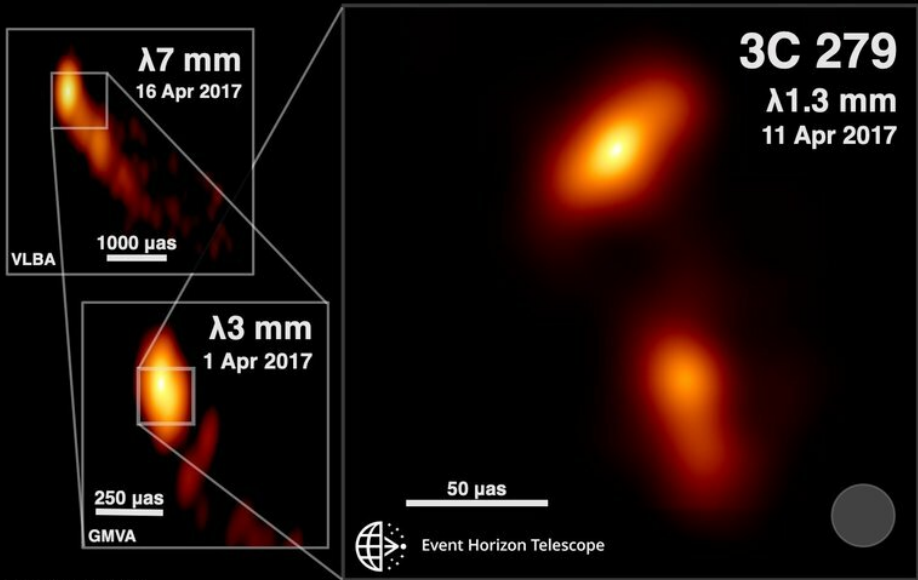
Astronomers Capture First Image of a Black Hole

Image Credit: EHT Collaboration

The Event Horizon Telescope (EHT) — a planet-scale array of eight ground-based radio telescopes forged through international collaboration — was designed to capture images of a black hole. Today, in coordinated press conferences across the globe, EHT researchers reveal that they have succeeded, unveiling the first direct visual evidence of a supermassive black hole and its shadow.

M87 Black Hole – Event Horizon Telescope





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